

# The John Jay College Expansion Project New York, NY



# Presentation Outline

- Project Information
- Existing Structural Systems
- Problem Statement and Solution
- Structural Design
- Architectural Studies
- Construction Studies
- Conclusions



# Project Information

## General Information

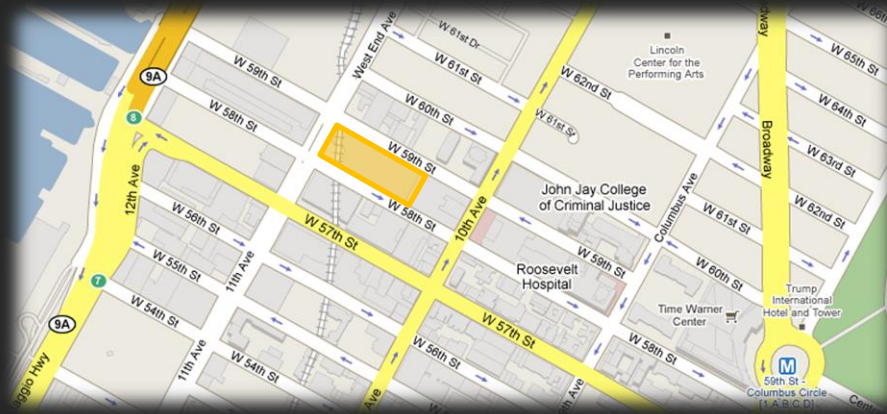
- Transform JJC of Criminal Justice into a 1-block urban campus
- Expansion to Existing Harren Hall
- 620,000 Square Feet
- \$ 457 Million
- 14 Story Tower
- 5 story Podium connecting tower to Harren Hall
- Design calls for:
  - Grand Cascade
  - Landscaped Podium Roof
  - Prefabricated Curtain Wall System



# Project Information

## Project Location

- 11<sup>th</sup> Avenue between 58<sup>th</sup> and 59<sup>th</sup> Street



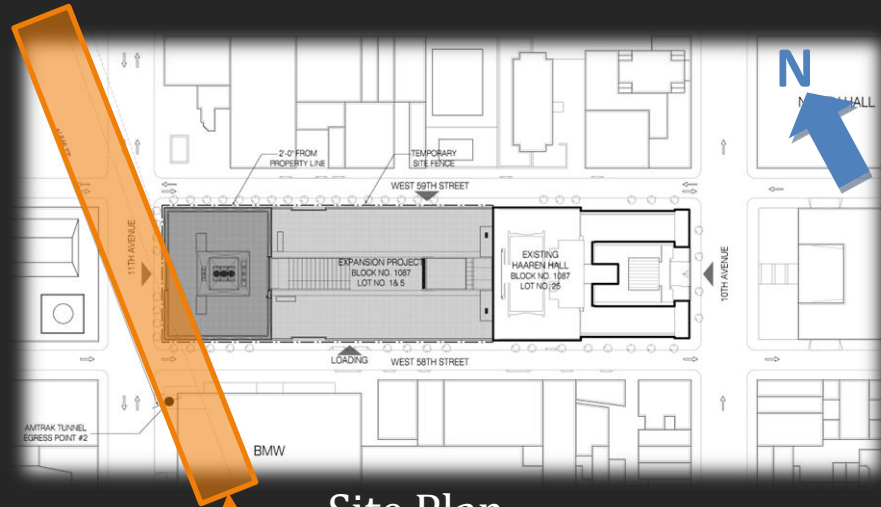
Michael Hopper – Structural Option  
AE Senior Thesis 2009

John Jay College Expansion Project  
New York, NY

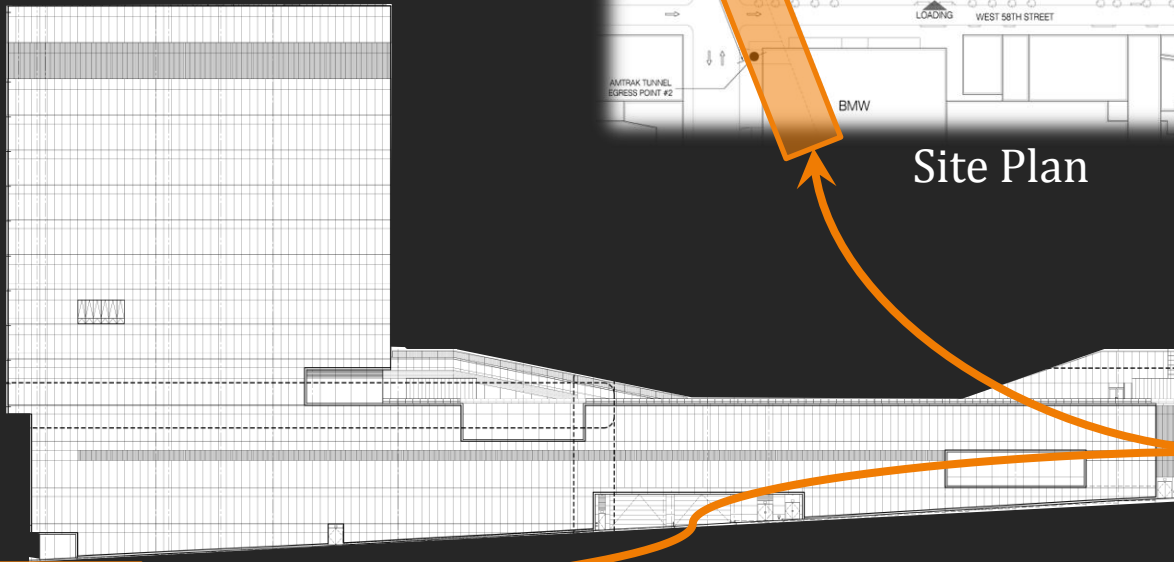


# Project Information

## Site Restriction



Site Plan



South Elevation

Amtrak tracks pass beneath the tower!

# Presentation Outline

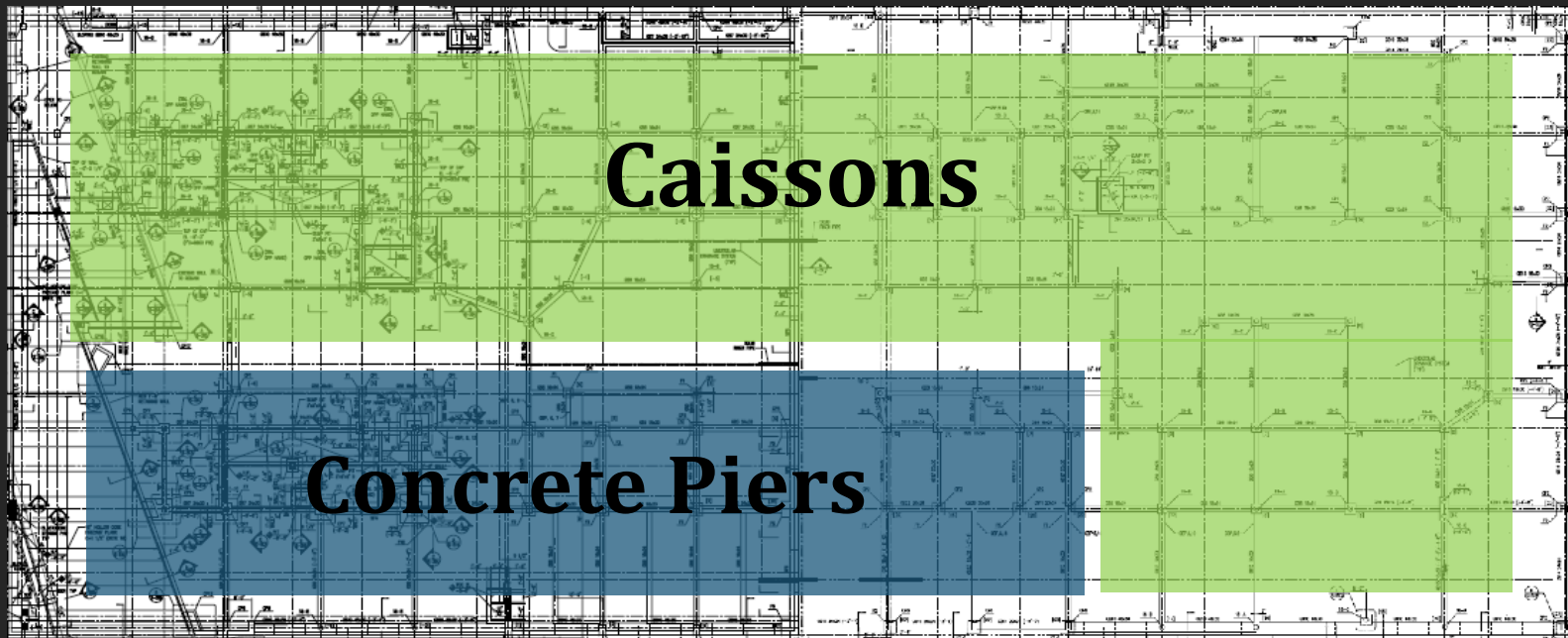
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# Existing Structural Systems

## Foundation

- Reinforced Concrete Caissons
  - 18" to 36" diameter embedded up to 14' in bedrock
  - Encased w/ ½" thick steel tubing
- Reinforced Concrete Piers
  - 20"x20" to 72"x42"
  - Typically extend 10' to individual column footings that bear on bedrock



# Existing Structural Systems

## Gravity System

- Composite Steel System
  - 3" metal decking spans 12'
  - 3 ¼" L.W. Concrete
- Typical Floor-to-Floor Height is 15'
- Typical Bay Spacing



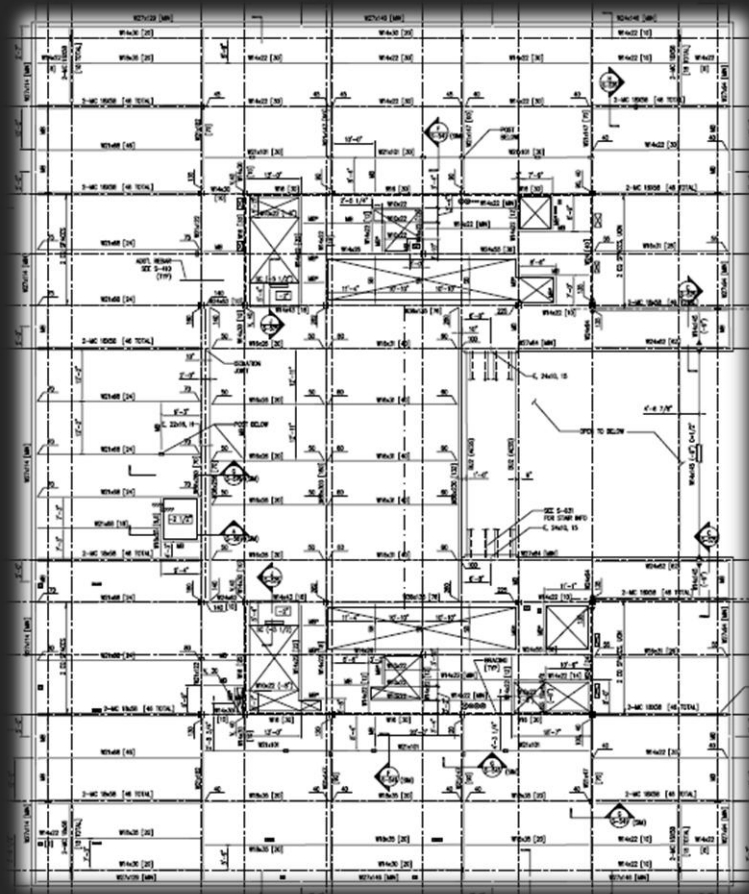
38'

26'

68'

26'

38'



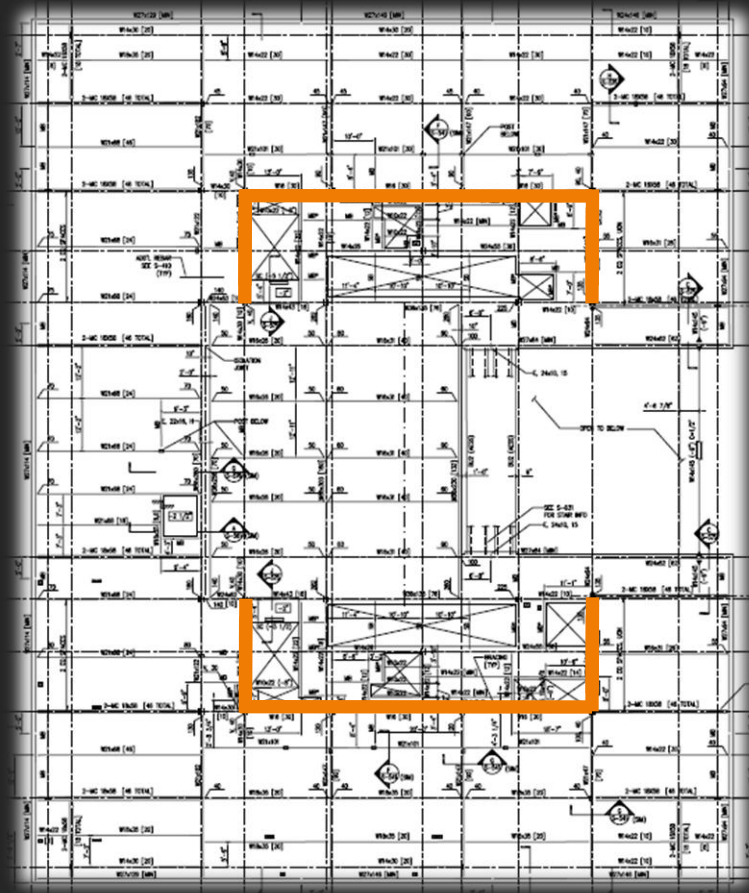
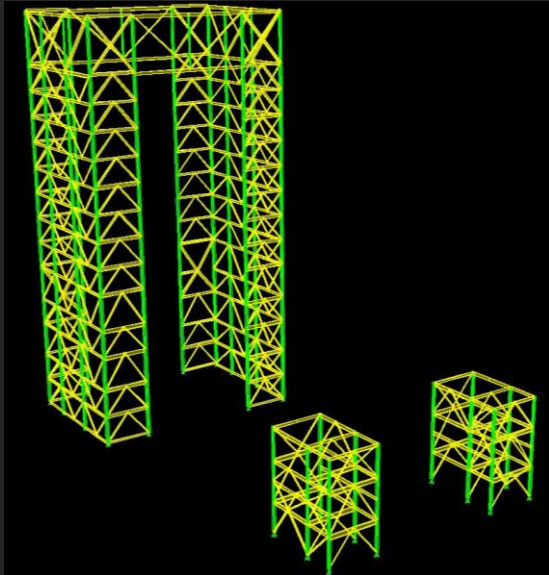
30'



# Existing Structural Systems

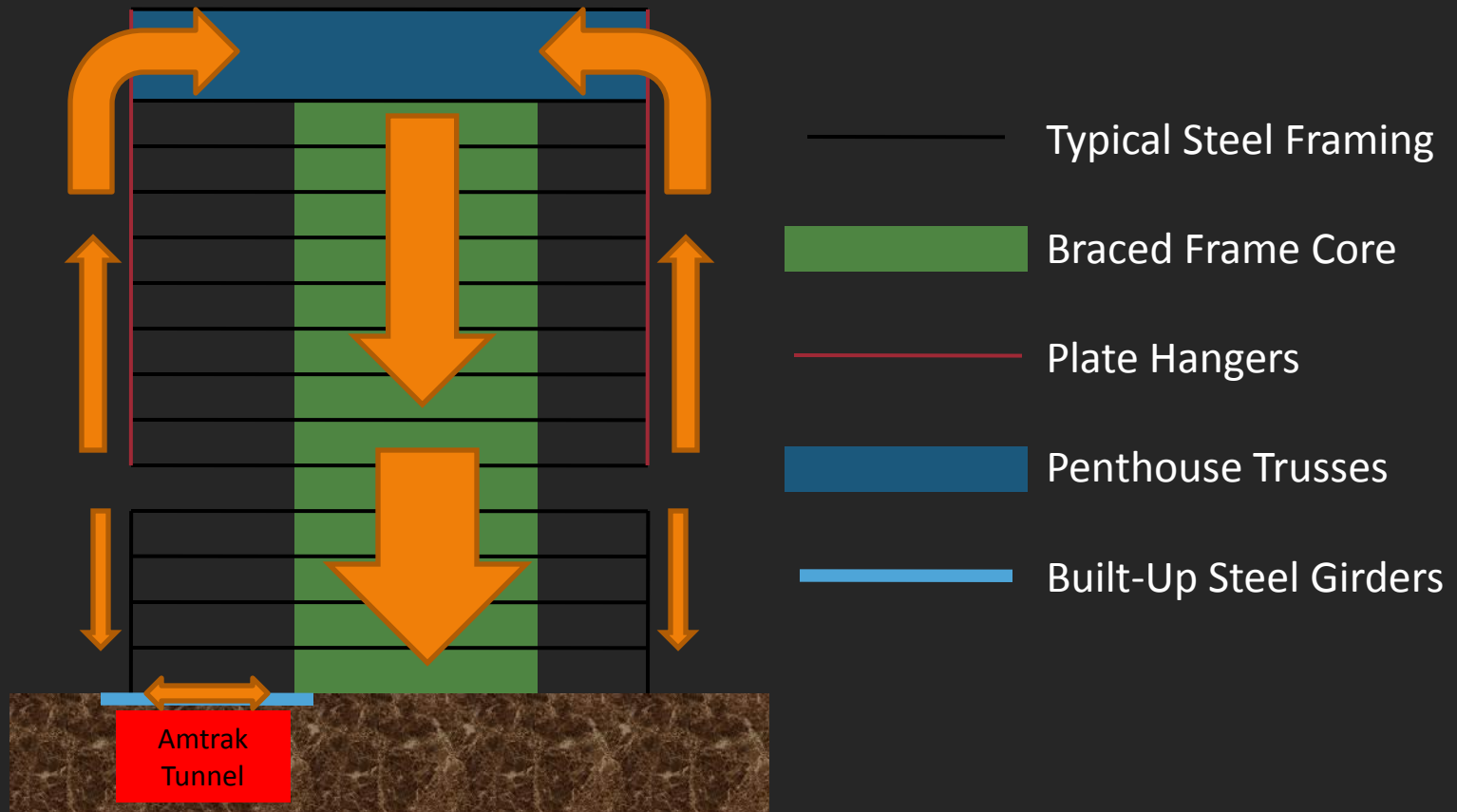
## Lateral Force Resisting System

- Concentrically Braced Frame Core
  - Braces range from HSS 6x6x3/8" to HSS 16x8x1/2"



# Existing Structural Systems

## Transfer System Solution



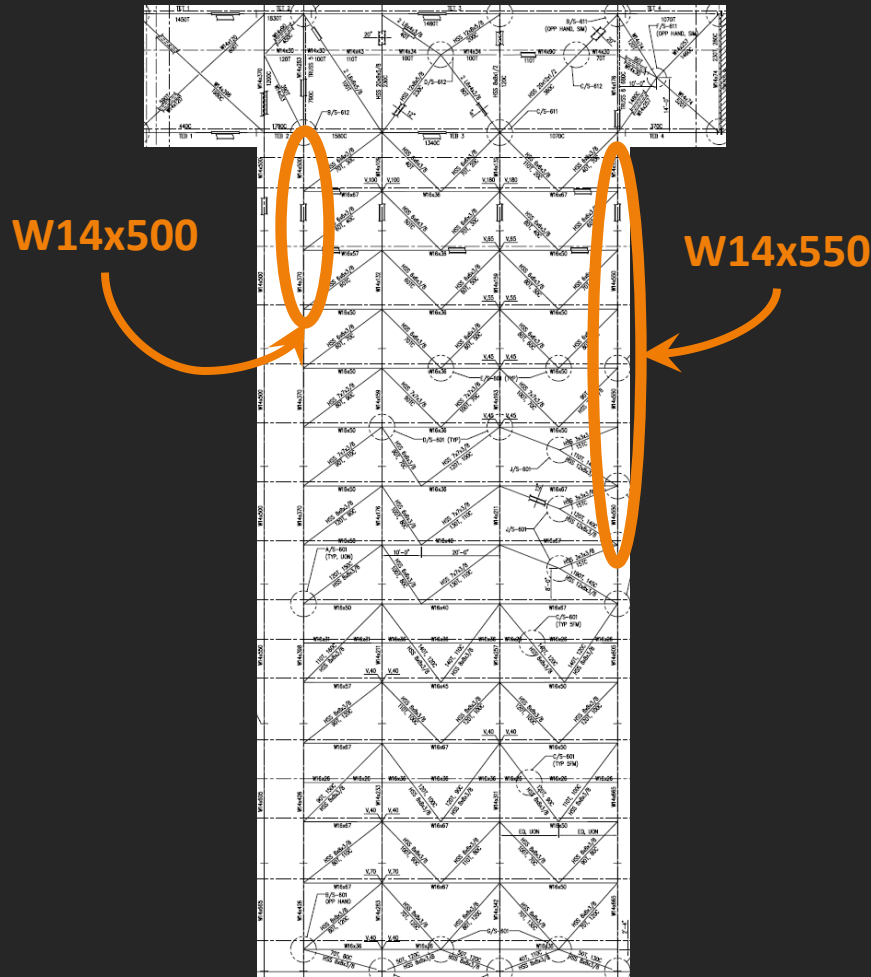
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# Problem Statement

## Inefficient Braced Frames



## Difficult Construction Methods

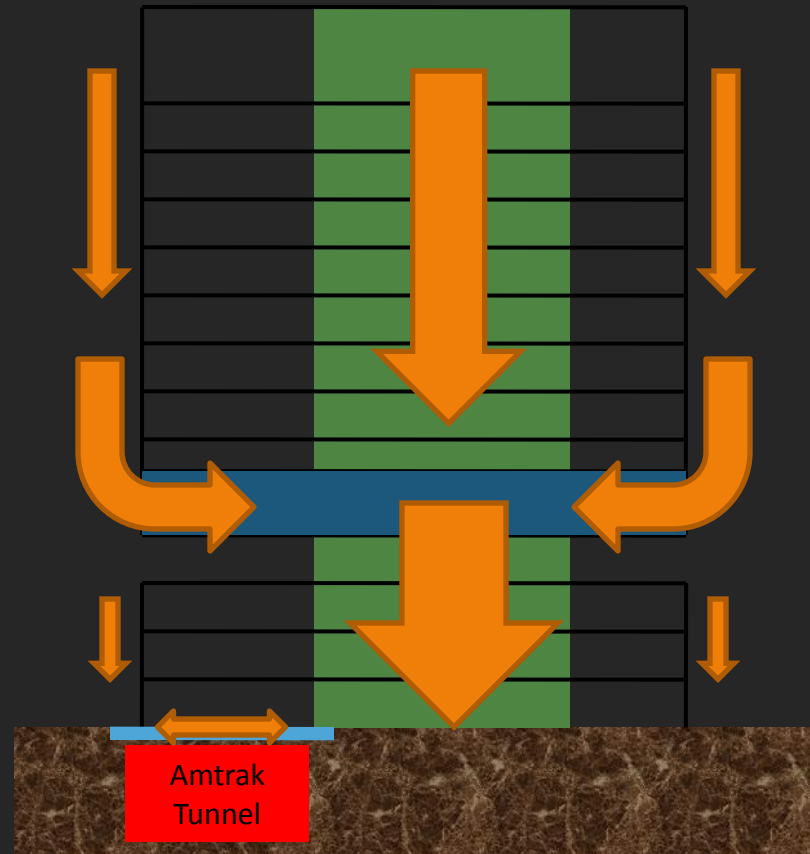
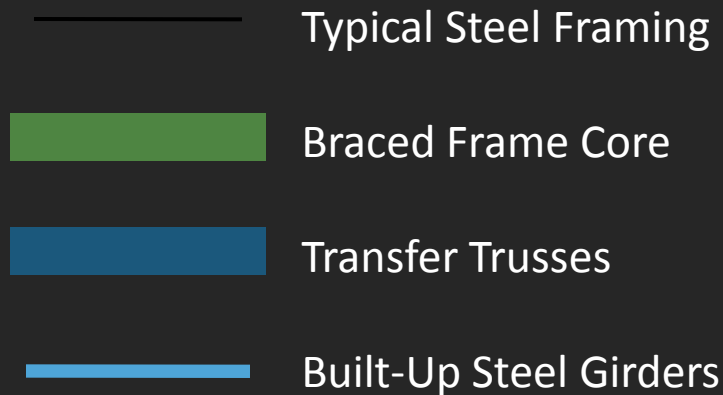
- Use of temporary columns
- Use of stiffened plate hangers to prevent buckling
- Built-up girders above Amtrak tracks must support construction loads of all levels until penthouse trusses are complete
  - Cannot place concrete deck until trusses are complete
- Expensive premiums charged



# Problem Solution

## Design a New Transfer System

- Optimize the Braced Frame Core
- Allow Traditional Construction Methods
- Gravity Loads are transferred more efficiently
  - All loads transferred down



# Project Goals



- Create a more constructible transfer solution than the existing design

- Design a series of transfer trusses which are architecturally exposed to building occupants



- Design custom built-up steel shapes for exposed truss members



- Perform an in-depth lateral analysis to develop an efficient design for the braced frame core



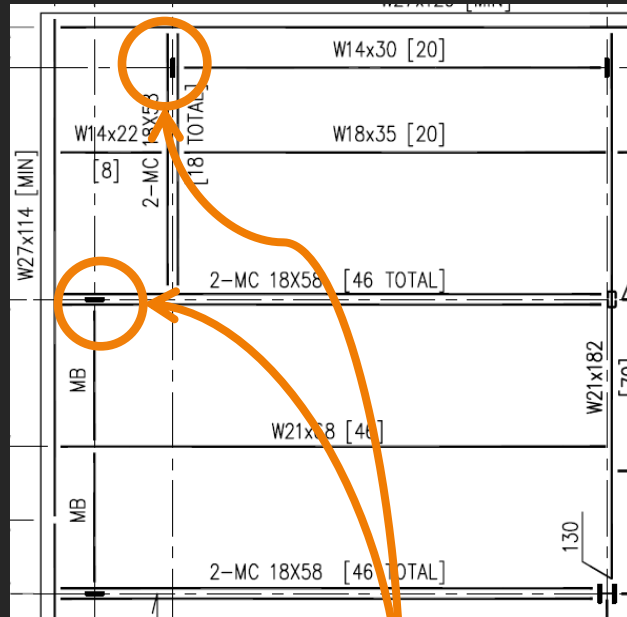
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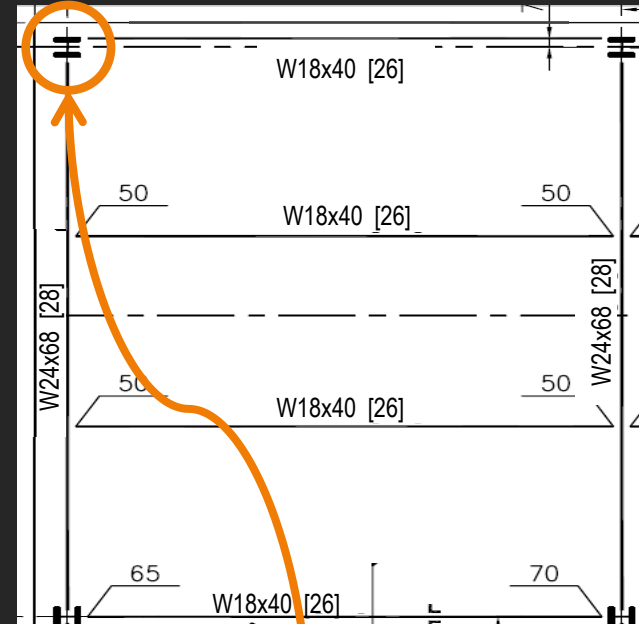
# Structural Depth Studies

## Corner Column Relocation and Floor Framing Design



Existing Plate Hanger Location

2 Plate Hangers



New Column Location

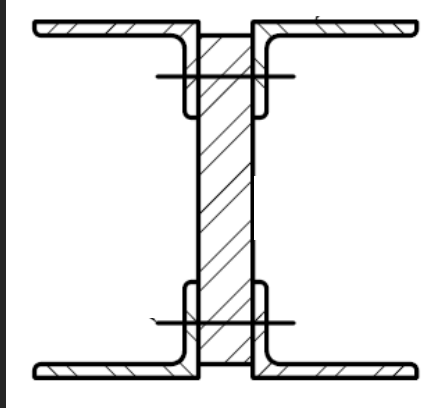
1 Corner Column



# Structural Depth Studies

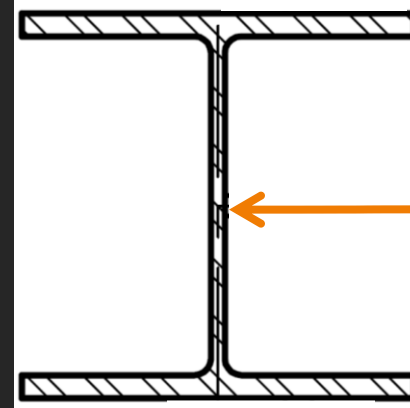
## Corner Column Relocation and Design

Existing Plate Hangers



- Total Weight: 107 kips
- Need to reinforce plates during construction to avoid buckling

New Columns

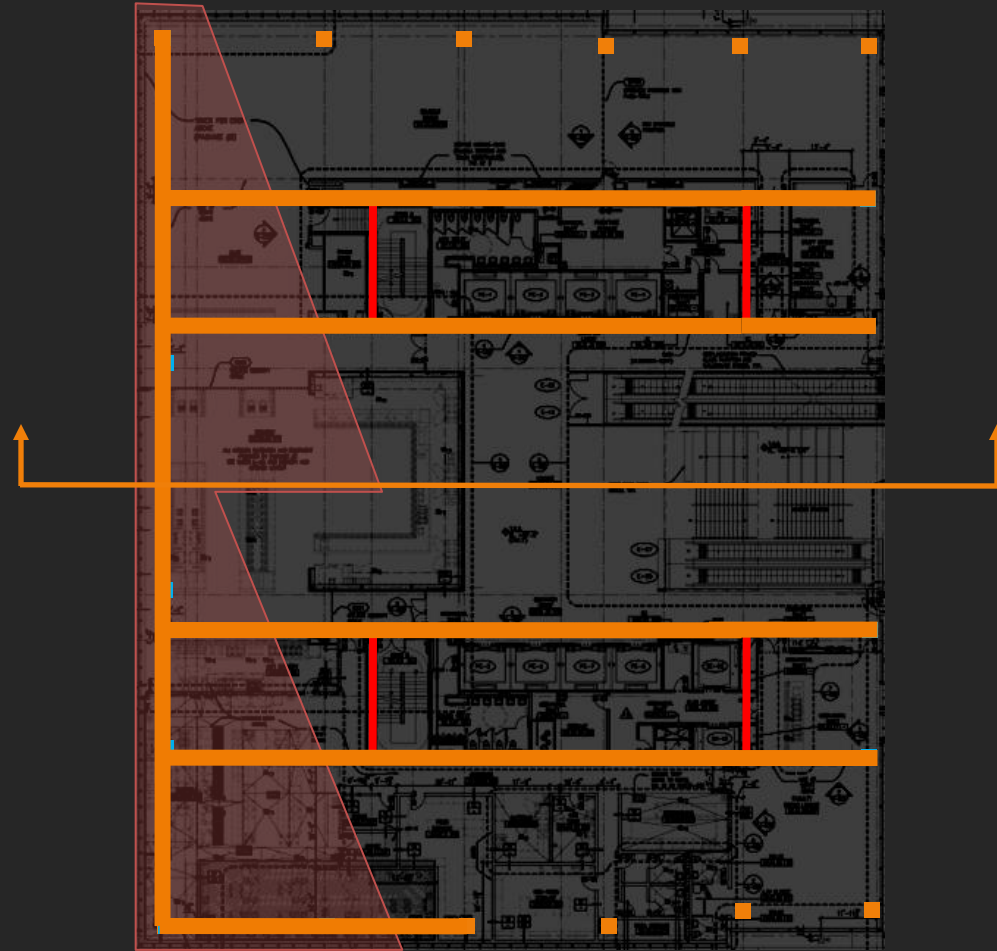


Easier to Construct

- Total Weight: 112 kips
- Typical steel framing can be used

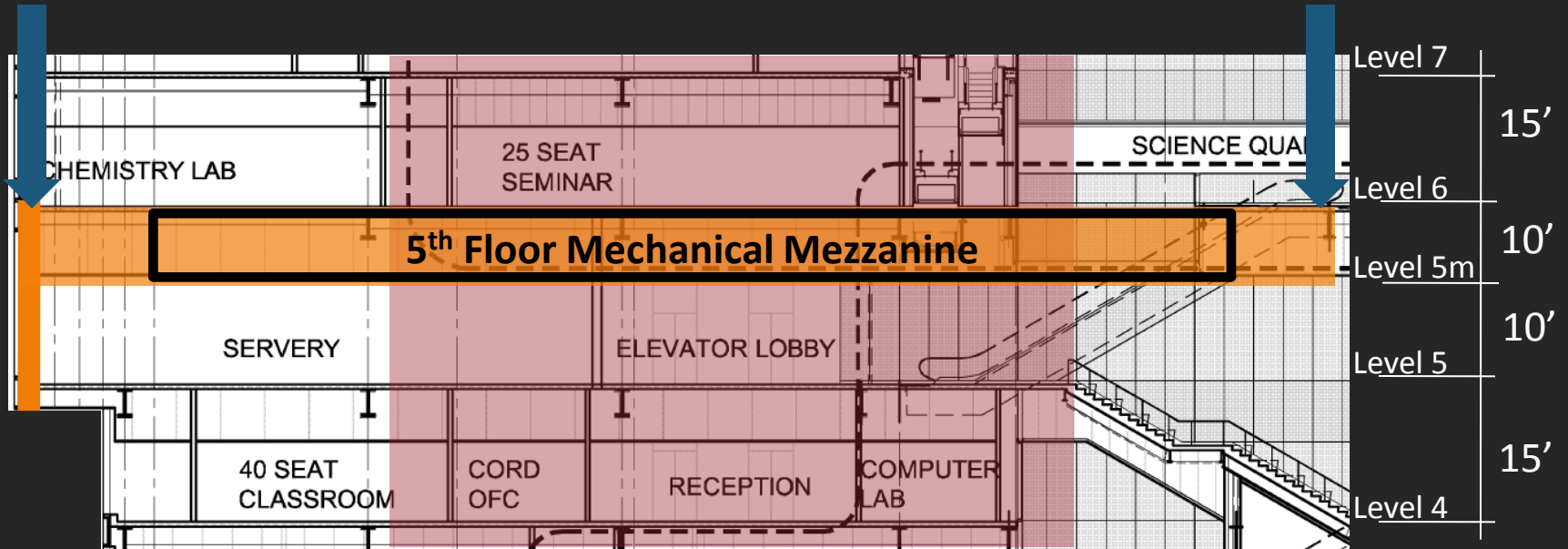
# Structural Depth Studies

## Transfer Truss Layout



# Structural Depth Studies

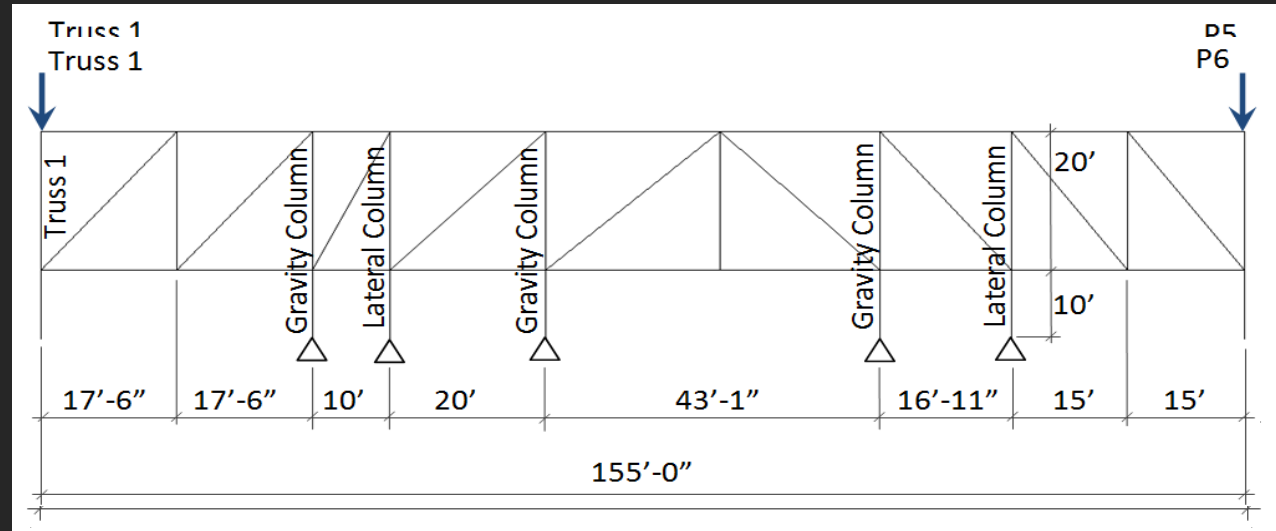
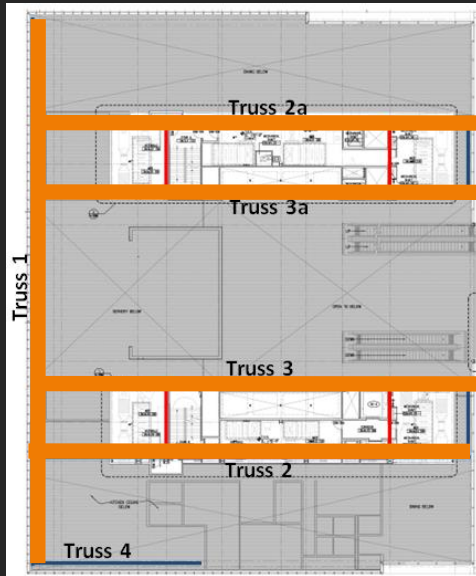
## Transfer Truss Layout



**20' Floor-to-Floor Height**

# Structural Depth Studies

## Transfer Truss Analysis



**Truss 1**

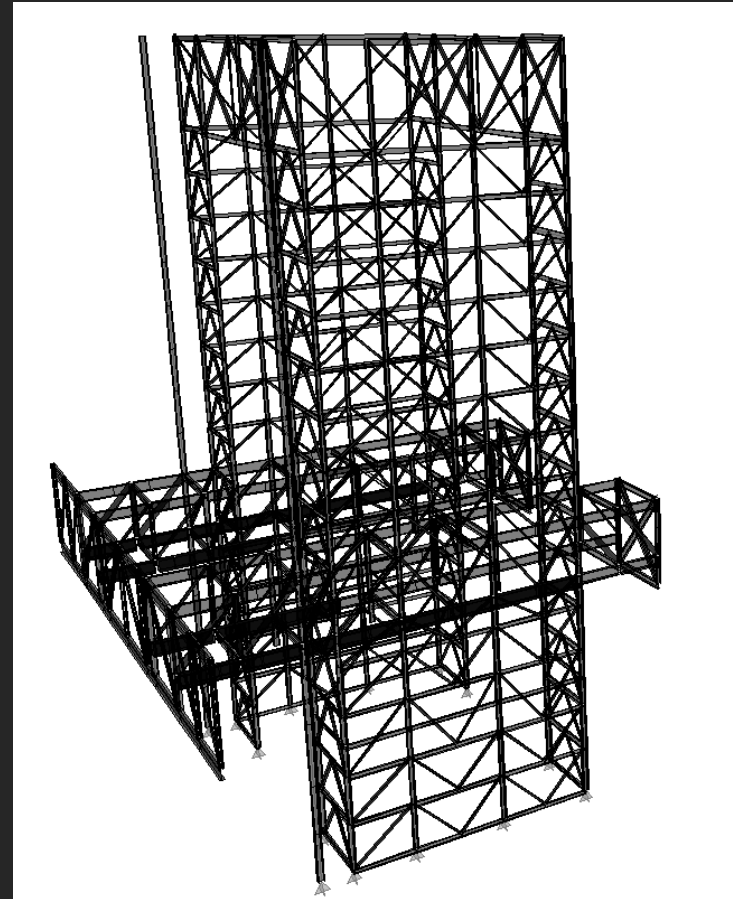
Loads	P1	P2	P3	P4	P5	P6	P7
Pu (kips)	804	1450	1668	876	1162	1753	1296



# Structural Depth Studies

## Truss Analysis – ETABS Gravity Model

- Diagonal web members are pinned at each end
- Top and bottom chords are continuous
- Floor diaphragms were not modeled
  - Top and bottom chords resist axial and bending forces
  - Chord unbraced lengths were taken as the distance between vertical web members
- Gravity Model was also used for deflection calculations

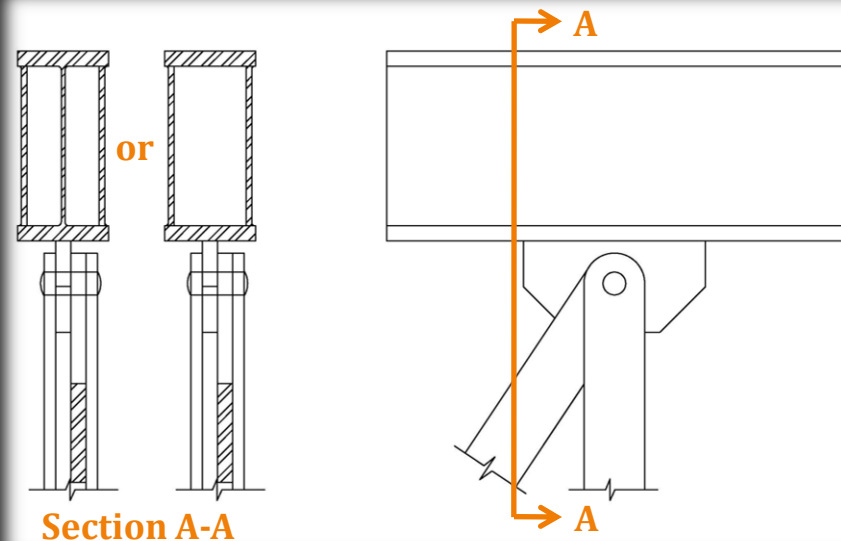


# Structural Depth Studies

## Truss Member Design



The Newseum "Megatruss"

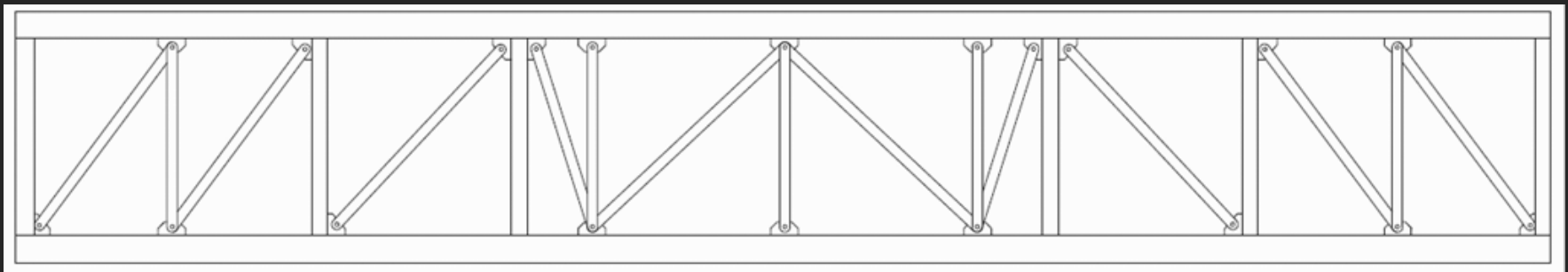


Desired Truss Details

**Design of all custom and built-up steel sections comply with the Specification of the 13<sup>th</sup> Edition AISC Steel Construction Manual**

# Structural Depth Studies

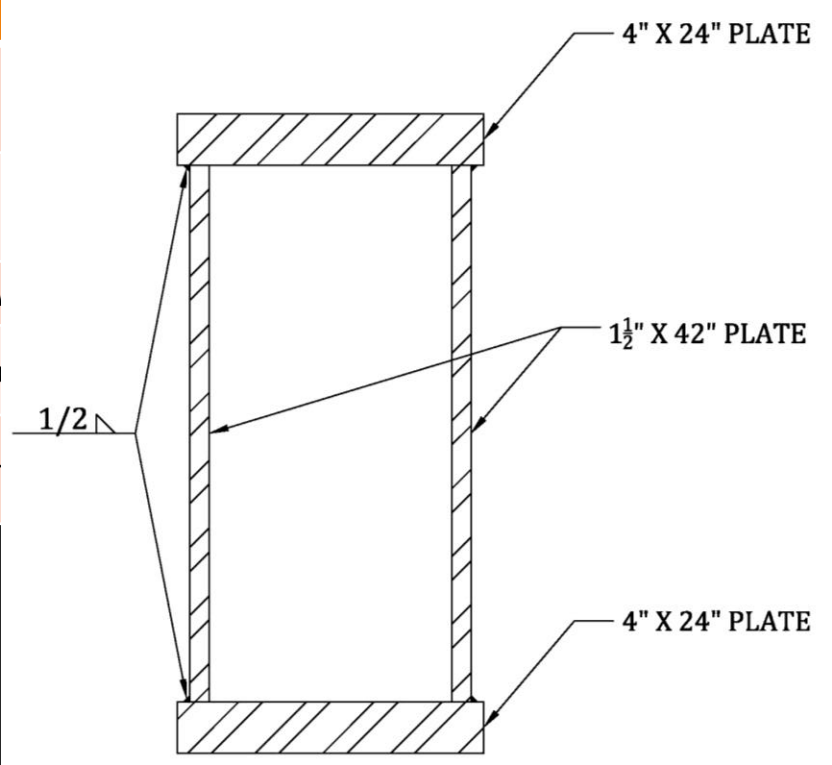
## Truss 1 Final Design



Member	Section	Design Forces
Top and Bottom Chords	W40x362	2700 kips (T) 1960 ft-kips
Web Tension Member	18 x 4 1/4" Plate	2430 kips
Web Compression Member	(2) 16 x 3" Plates stitched at 2'	1960 kips
Common Truss Members	W36x441	3410 kips (C) 680 ft-kips

# Structural Depth Studies

## Truss 2 Final Design

Member	Section	Design Forces
W Web Cor	 <p>4" X 24" PLATE</p> <p>1 1/2" X 42" PLATE</p> <p>4" X 24" PLATE</p> <p>1/2"</p>	5800 kips (T) 4500 ft-kips
		6000 kips (C) 9500 ft-kips
		4850 kips 3370 kips 50" deep x 24" wide
		3410 kips (C) 680 ft-kips Weighs 1082 lbs

# Structural Depth Studies

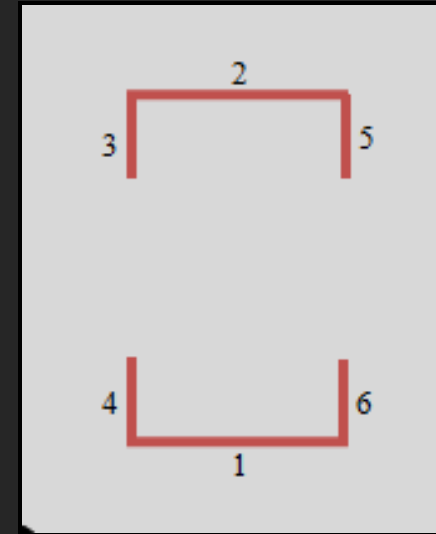
## Transfer Truss Comparison

Criteria	Thesis Transfer System	Existing Transfer System
Number of Transfer Trusses	6	10
Perimeter Columns Transferred	11/20 (55%)	24/24 (100%)
Total Web Members	102	206
Avg. Truss Weight (kips)	230	152
Interior Truss Height	20'-0"	30'-0"
Number of Levels Being Transferred w/ Trusses	11	10

# Structural Depth Studies

## Lateral Analysis and Design

- Tower Braced Frame Core Re-design
- ETABS Lateral Model
  - Floors modeled as rigid diaphragms
  - Lateral loads distributed based on relative stiffness of each braced frame
- Lateral loads determined using ASCE 7-05
  - Wind: Method 2 of Chapter 6
  - Seismic: ELFP of Chapter 11 (SDC: B)
  - Wind governed for strength and serviceability

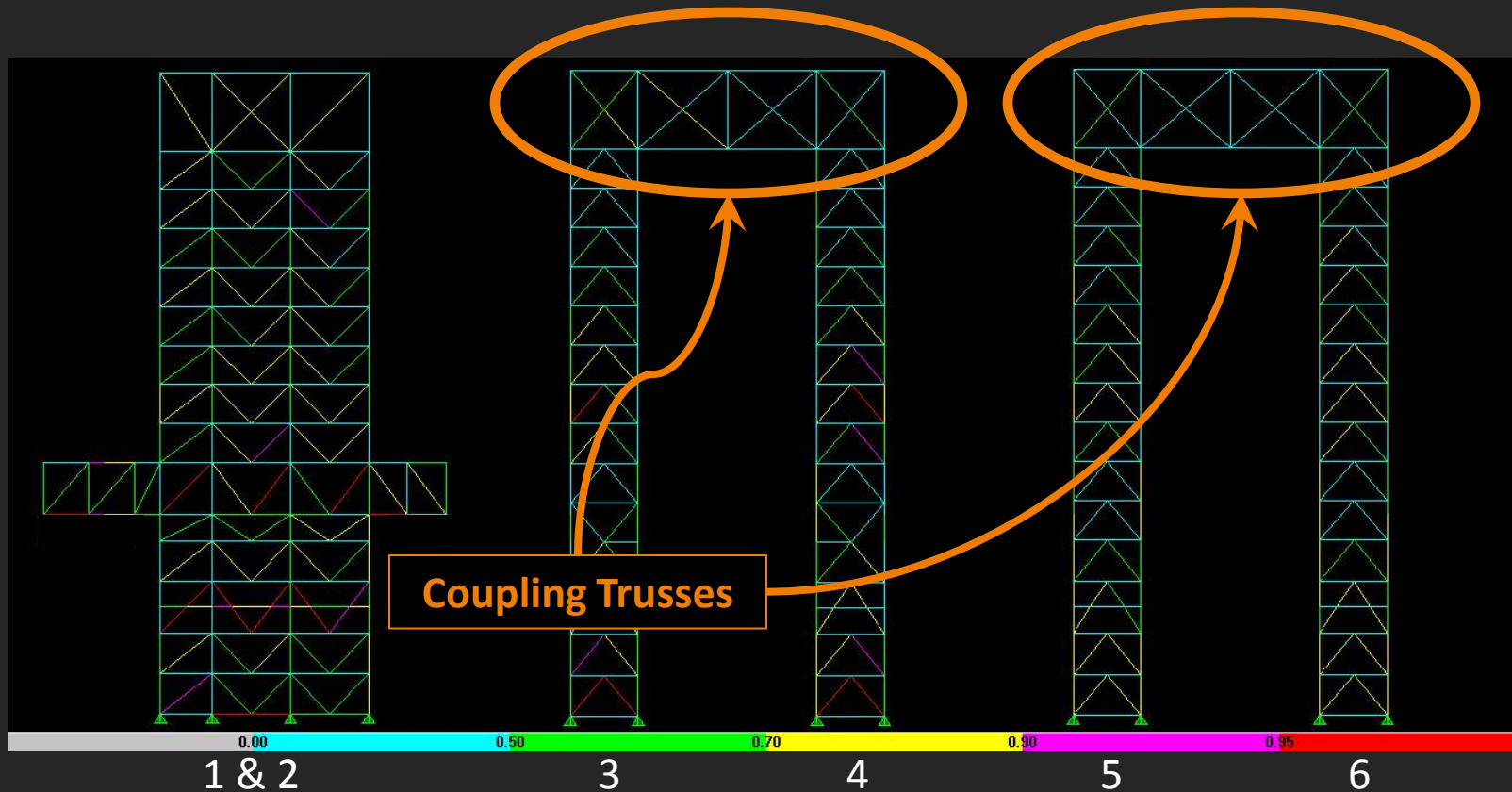




# Structural Depth Studies

## Lateral Analysis and Design

### Braced Frame Configurations and Demand-to-Capacity Ratios



# Structural Depth Studies

## Lateral Analysis and Design – Braced Frame 1 & 2

### Existing Typical Members

Level	Column	Brace	Girder
1 - 3	W14x665	HSS 8x8x3/8	W16x67
4-7	W14x605	HSS 8x8x3/8	W16x45
7-10	W14x550	HSS 7x7x3/8	W16x36
11-14	W14x550	HSS 6x6x3/8	W16x36

**Largest Brace is an HSS 8x8x3/8**

### Re-designed Typical Members

Level	Column	Brace	Girder
1 - 3	W14x455	HSS 8x8x3/8	W16x67
4-7	W14x455	HSS 8x8x5/8	W16x45
7-10	W14x176	HSS 8x8x3/8	W16x36
11-14	W14x99	HSS 6x6x3/8	W16x36

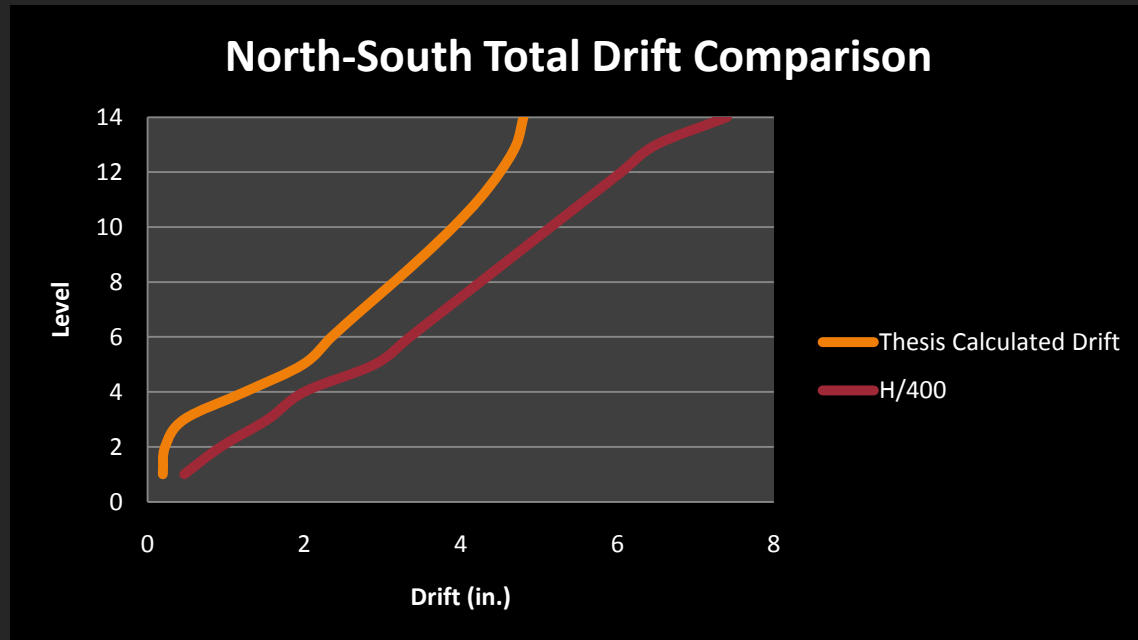
**Largest Brace is an HSS 20x12x5/8**

**New braced frame design resulted in saving  
71 tons of steel in columns**

# Structural Depth Studies

## Lateral Drift – ASCE 7-05

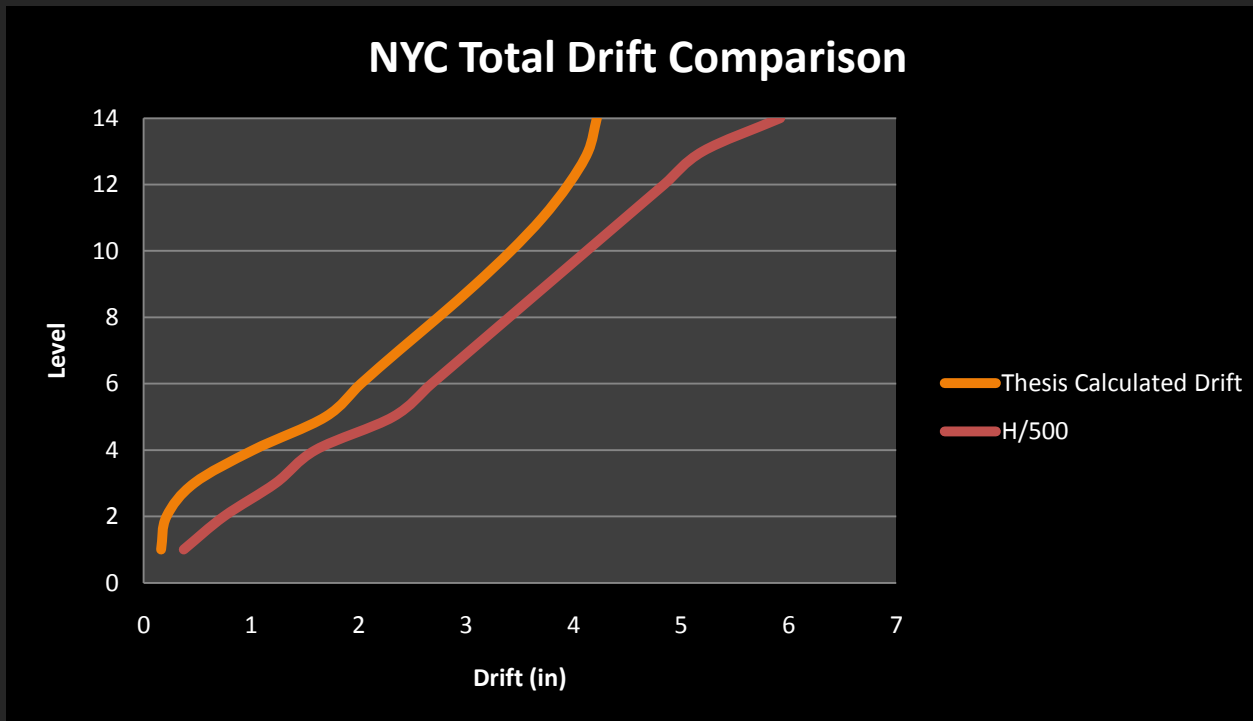
- Calculated Lateral Drifts
  - Wind:  
LC:  $0.7W$  (App. C)
  - Seismic:  
 $\delta_{xe} C_d / I$
- Lateral Drift Limitations
  - Wind:  
 $H/400$
  - Seismic:  
 $0.015h_{sx}$
- Lateral Drifts due to wind governed
  - Maximum drift is in N-S direction



# Structural Depth Studies

## Lateral Drift – New York City Building Code

- Necessary to compare re-design to the original design criteria

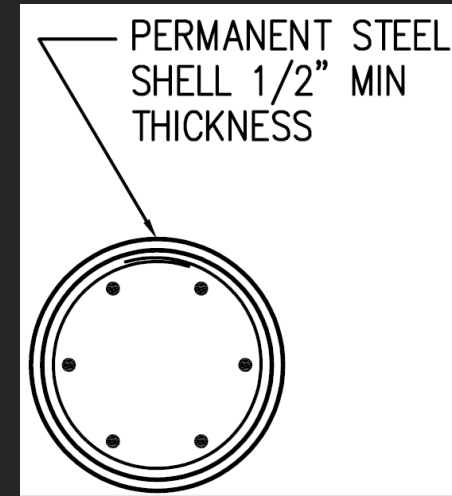


# Structural Depth Studies

## Foundation Impacts

- Perimeter columns not transferred using 5<sup>th</sup> level trusses now extend to the foundation
- Existing concrete caissons support 5 levels of gravity load, where the new design calls for 14 levels of gravity loads

	Existing	Thesis
Diameter	18"	36"
Reinforcement	(7) #14 Bars	(11) #14 Bars



**Impacts are minimal as only 7 caissons need changed**

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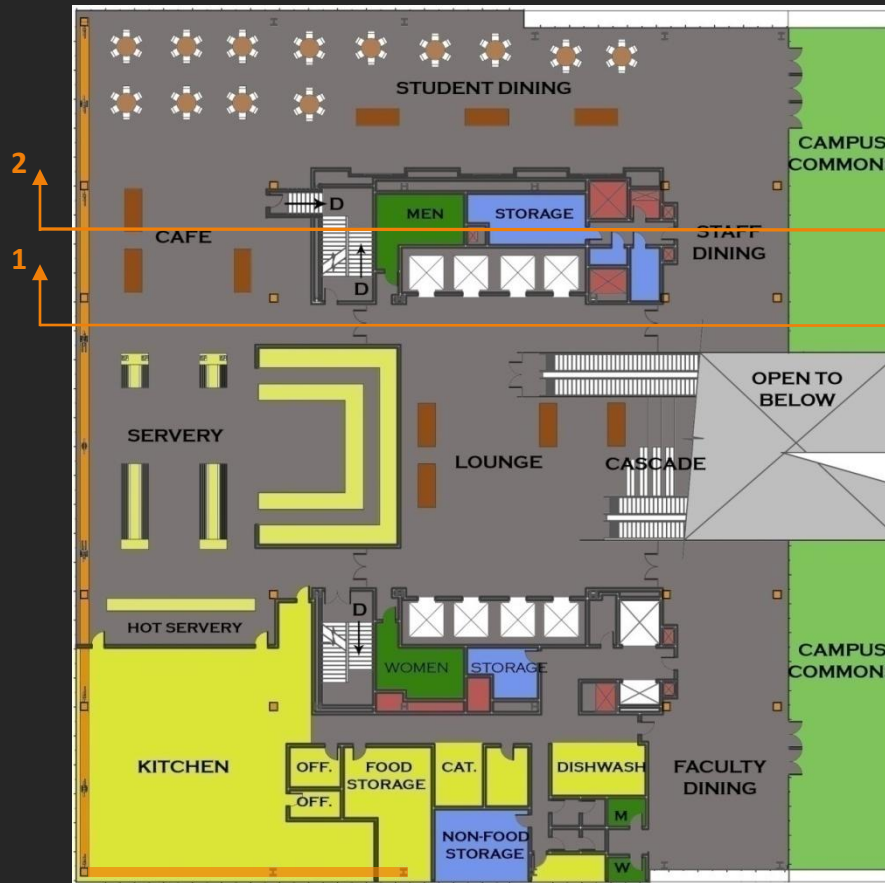
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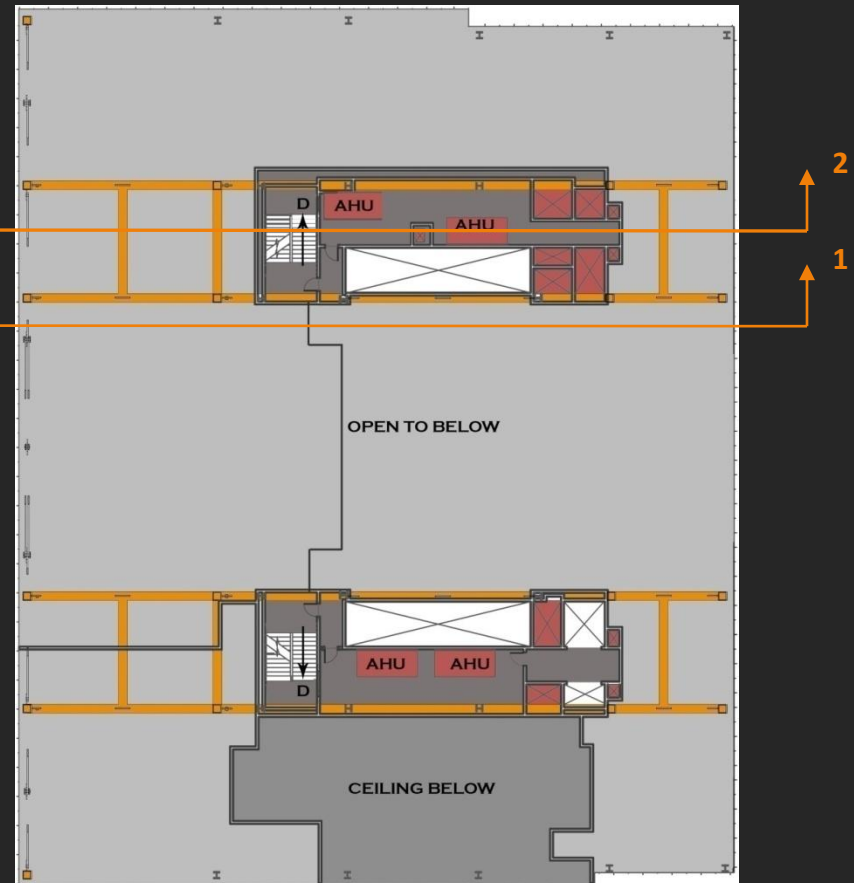


# Architectural Breadth Studies

## 5<sup>th</sup> Level Floor Plan

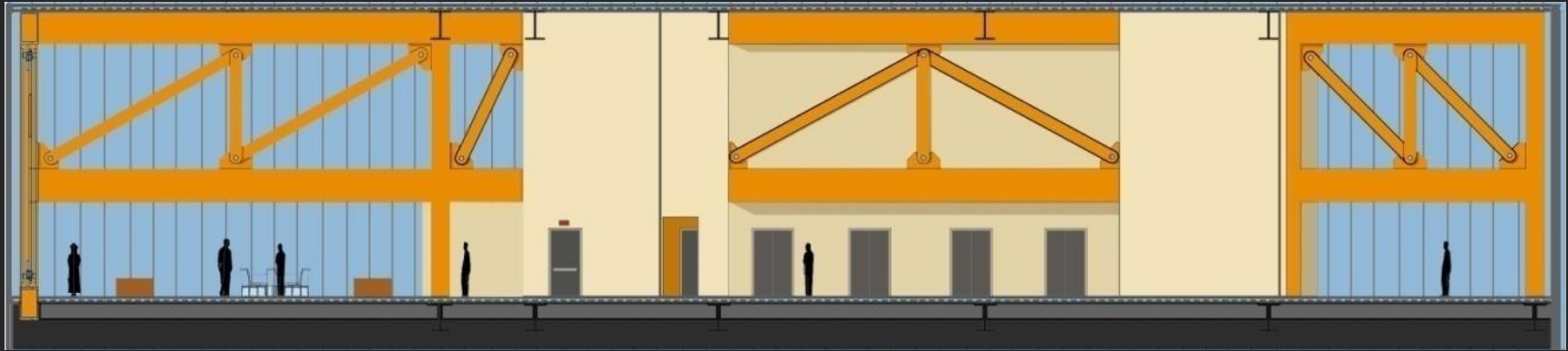


## 5<sup>th</sup> Level Mezzanine Floor Plan

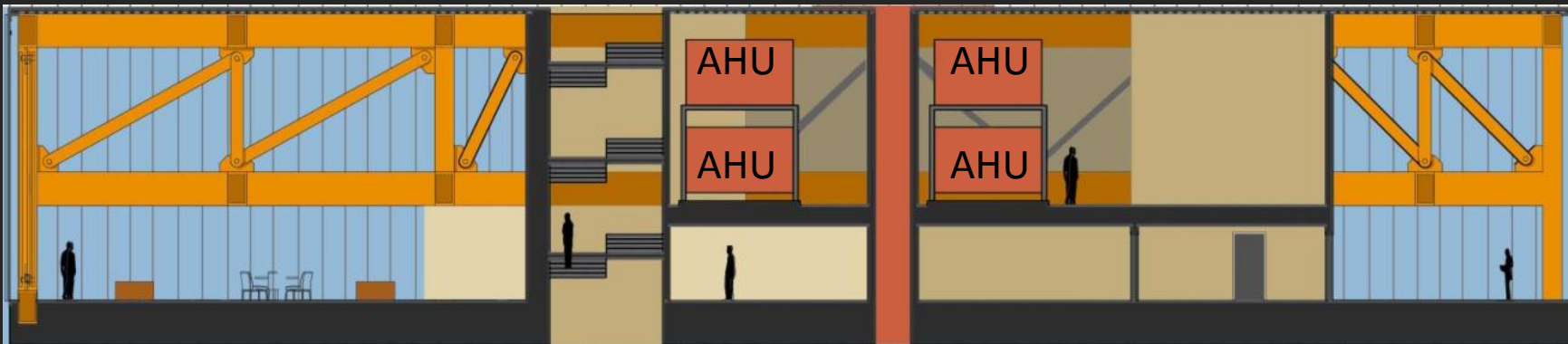


# Architectural Breadth Studies

## Section 1



## Section 2



# Architectural Breadth Studies

## Interior Renderings



# Architectural Breadth Studies

Existing Exterior  
Renderings



Michael Hopper – Structural Option  
AE Senior Thesis 2009

John Jay College Expansion Project  
New York, NY



# Architectural Breadth Studies

New Exterior  
Renderings



Michael Hopper – Structural Option  
AE Senior Thesis 2009

John Jay College Expansion Project  
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# Construction Management Breadth Studies

## Cost Comparison

	Thesis (kips)	Existing (kips)
Cost of Steel	\$ 5.83 Million	\$ 6.24 Million
Increased Curtain Wall Cost	\$ .820 Million	--
Preconstruction Costs	\$ 0.069 Million	\$ 0.114 Million
Dismantle Temporary Supports	--	\$ 0.125 Million
Hydraulic Jacks	--	\$ 0.125 Million
<b>Total</b>	<b>\$ 6.71 Million</b>	<b>\$ 6.60 Million</b>

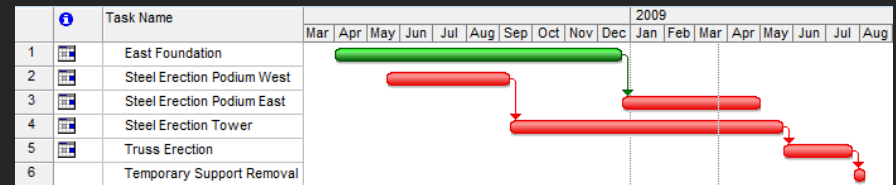
**Both systems cost about the same**

# Construction Management Breadth Studies

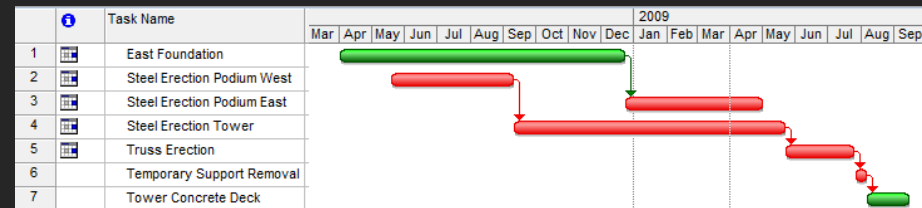
## Schedule Comparison – Existing Sequence



**Steel Erection Time: 63 Weeks**



**Total Superstructure Time: 70 Weeks**

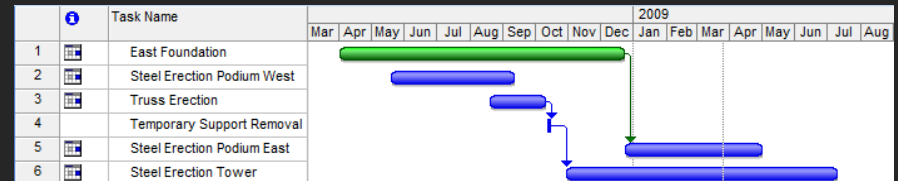


# Construction Management Breadth Studies

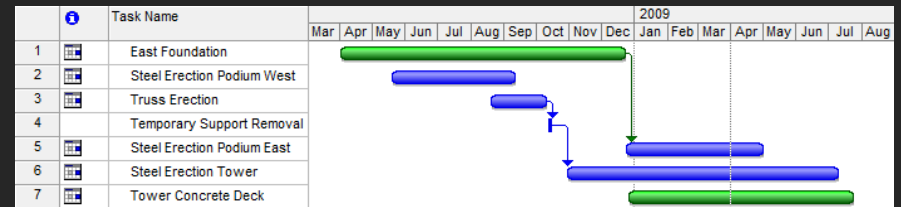
## Schedule Comparison – New Sequence



**Steel Erection Time: 60 Weeks**



**Total Superstructure Time: 64 Weeks**



# Construction Management Breadth Studies

## Construction Conclusions

	Thesis Transfer System	Existing Transfer System
Structural System Cost	\$ 5.89 Million	\$ 6.60 Million
Total Cost	\$ 6.71 Million	\$ 6.60 Million
Steel Erection Schedule (Weeks)	60	63
Entire Superstructure Schedule (Weeks)	64	70

- Steel erection tops out 3 weeks earlier using the new transfer system
- Total superstructure schedule is 6 weeks less using the new transfer system
- **Less trusses and truss members**
- **Eliminating the use of temporary supports in tower construction**
- **Using typical steel framing**

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# Conclusions and Recommendation

- Braced Frame Core was optimized by relocating the transfer trusses to the 5<sup>th</sup> level

- Exposed steel transfer trusses with custom steel members compliment the 5<sup>th</sup> level dining commons

- A more constructible structure was achieved

Recommendation:

**Use the new transfer solution**





# Acknowledgements

A special thanks to:



Jason Stone, PE  
Patrick Hopple



Anthony Gervaise, LEED AP



Ramesh Rastogi

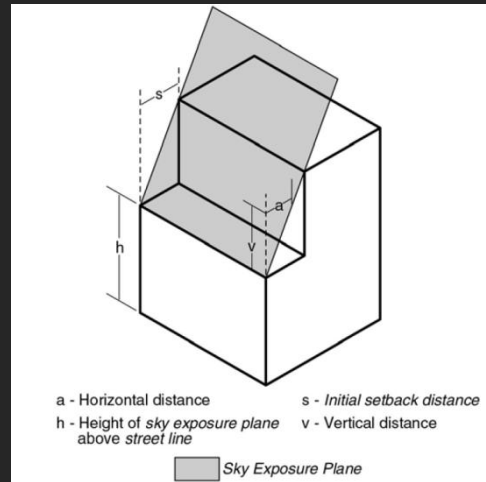


I also would like to thank my friends and family for their support over the past year, this project would not have been possible without you.

# Questions?



# Building Height Limitations



- C6-2 Special Purpose Zone – **No Maximum Building Height**
- However, NYC has building setback requirements
- Sky Exposure Plane
  - For a C6-2 Zone, vertical to horizontal ratio is 7.6 : 1
  - Existing design requires a setback of 20' at the roof and only 15' is provided
  - Assumed that a variance was obtained or the zone was changed



# Load Combinations

## ASCE 7 – 05 Load Combinations

1.  $1.4D$
2.  $1.2D + 1.6L + 0.5L_r$  ← Transfer System Members
3.  $1.2D + 1.6L_r + (L \text{ or } 0.8W)$
4.  $1.2D + 1.6W + L + 0.5L_r$  ← Braced Frame Members
5.  $(1.2 + 0.2S_{DS})D + E + L$
6.  $0.9D + 1.6W$
7.  $(0.9 - 0.2S_{DS})D + E$

# Scheduling Assumptions

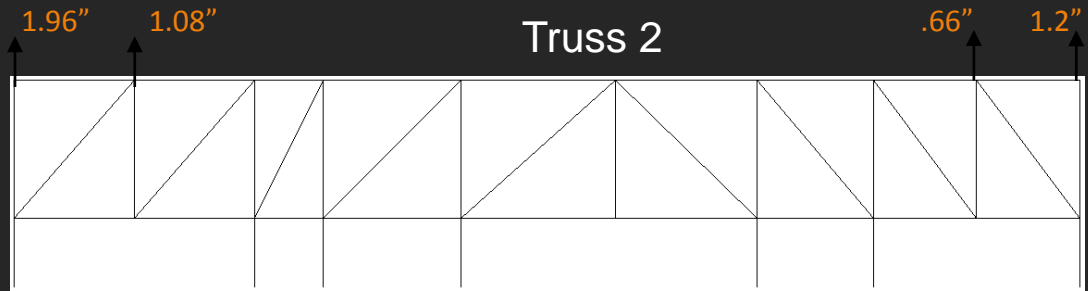
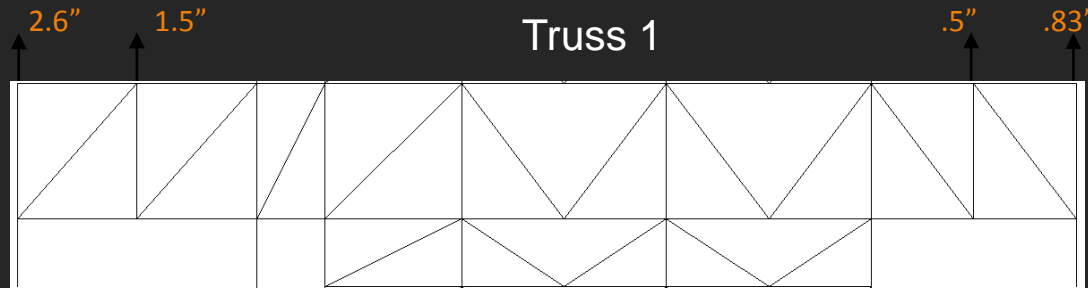
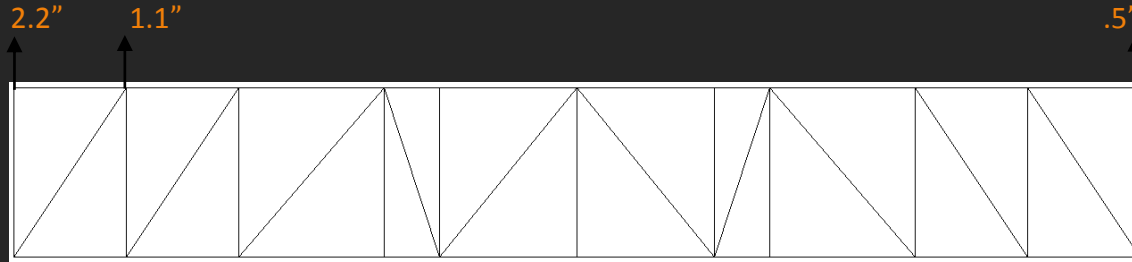
Activity	Thesis (Duration in Days/Level)	Existing (Duration in Days/Level)
Erect Columns	1	1
Erect Braced Frames	1	1
Erect Typical Floor Framing	7	7
Decking and Detailing	10	10
Erect Temporary Columns	1	1
Erect Reinforced Plate Hangers	N/A	1
Erect Truss Bottom Chords	3	4
Erect Truss Top Chords	2	4
Erect Truss Web Members	3	6
Detail and Plum Trusses	5	10
Remove Temporary Columns/Reinforced Plates	1 <sup>1</sup>	5 <sup>1</sup>
Placing Concrete Decking	10 <sup>2</sup>	2 <sup>3</sup>

<sup>1</sup> - Unit is Total Days

<sup>2</sup> - Includes duration of embeds, box outs, rebar, and placing concrete

<sup>3</sup> - Includes placing concrete

# Truss Cambers and Deflections



Truss 3

Maximum Live Load Deflections

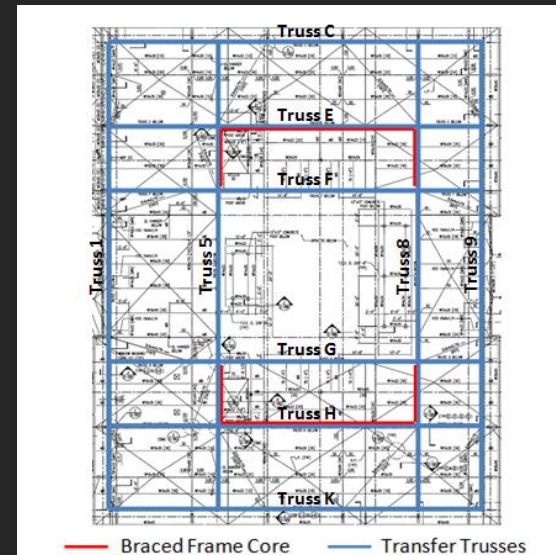
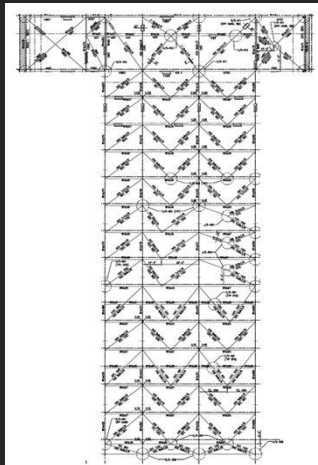
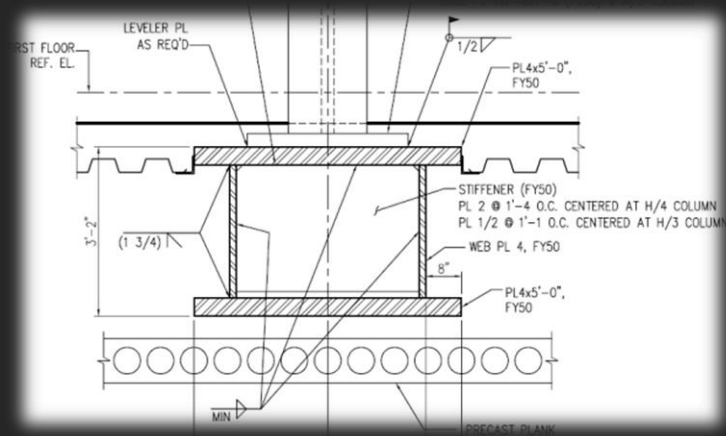
Truss	L	$0.5\Delta_L$	(L/250)
	(ft)	(in)	(in)
1	40	1.41	1.92
2	35	0.73	1.68
2a	35	0.35	1.68
3	35	0.53	1.68
3a	35	0.36	1.68



# Existing Structural Systems

## Transfer System Solution

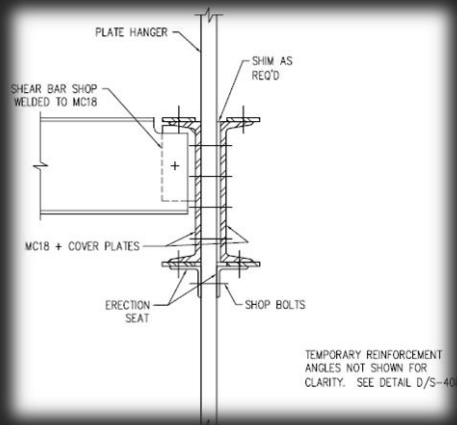
- Floors 1 – 5 transferred using built-up girders
- Floors 6 – Roof are hanging and are transferred at the penthouse level using trusses



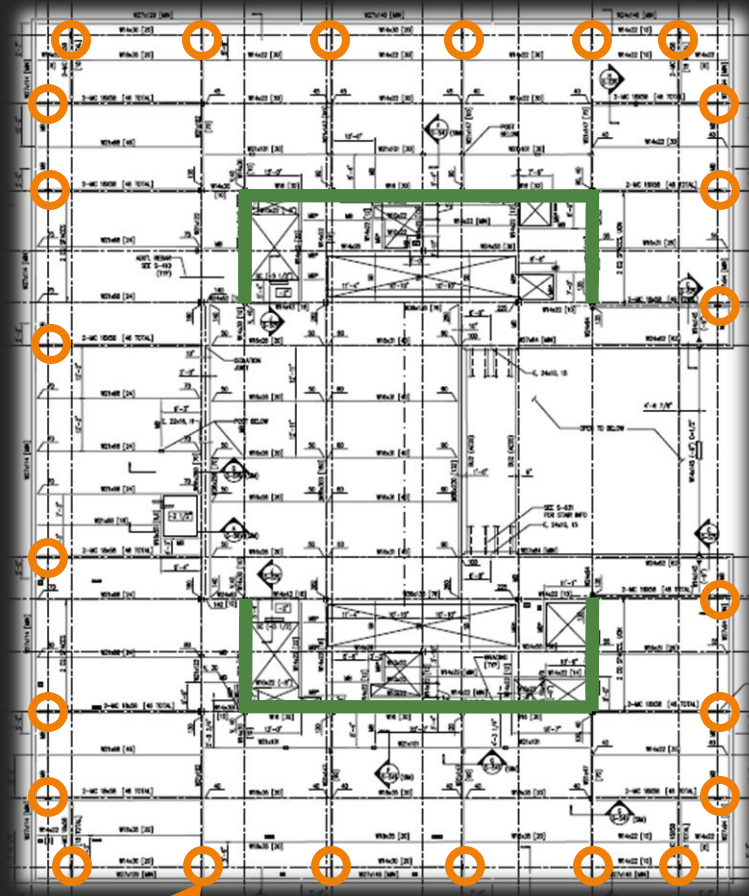
# Existing Structural Systems

## Transfer System Solution

- Floors 6 – Penthouse use perimeter plate hangers instead of columns

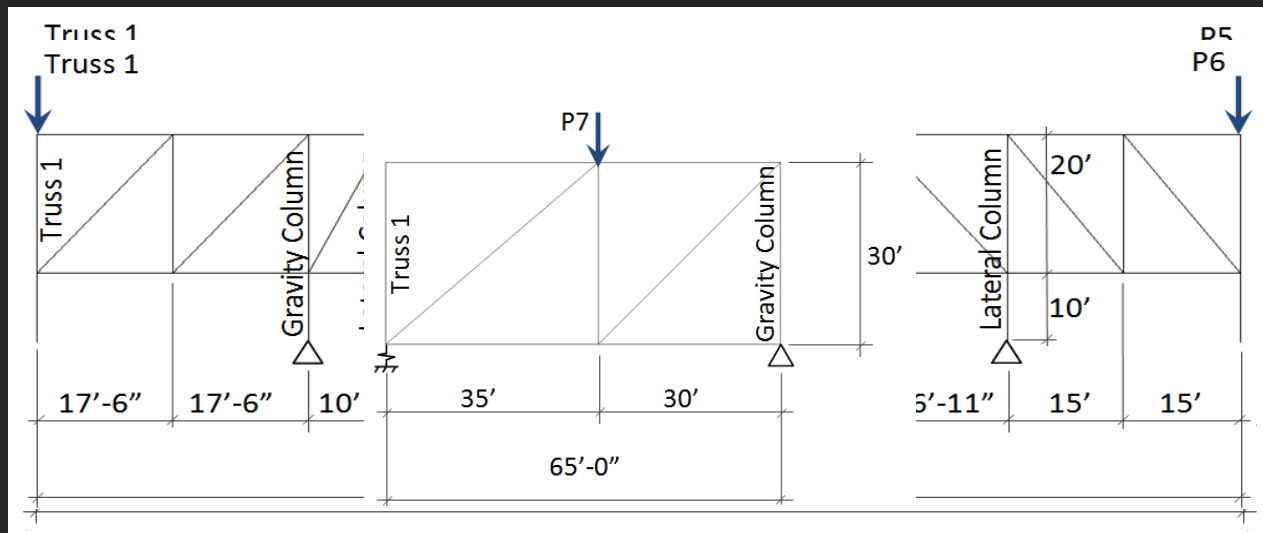
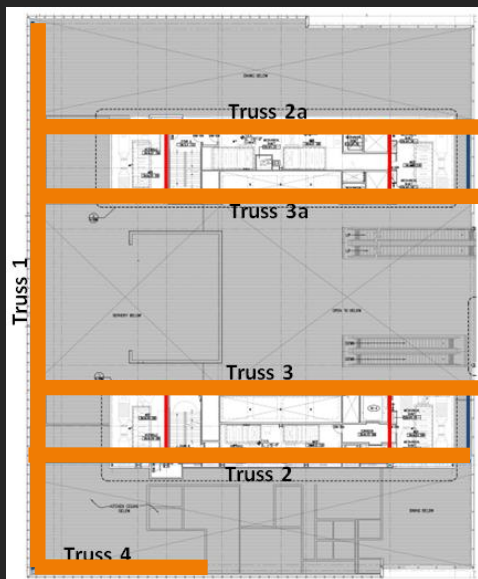


Perimeter Plate  
Hangers



# Structural Depth Studies

## Transfer Truss Analysis



**Truss 1**

Loads	P1	P2	P3	P4	P5	P6	P7
Pu (kips)	804	1450	1668	876	1162	1753	1296

# Structural Depth Studies

## Lateral Analysis and Design

### Existing Braced Frame 3 & 4

Level	Column	Brace	Girder
1 - 3	W14x426	HSS 8x8x3/8	W24x84
4-7	W14x398	HSS 20x8x1/2	W16x67
7-10	W14x370	HSS 8x8x3/8	W16x36
11-14	W14x500	HSS 16x8x1/2	W16x36

### Re-designed Braced Frame 3 & 4

Level	Column	Brace	Girder
1 - 3	W14x426	HSS 12x8x5/8	W24x84
4-7	W14x550	HSS 20x8x5/8	W16x67
7-10	W14x132	HSS 8x8x1/2	W16x36
11-14	W14x132	HSS 12x8x3/8	W16x36

# Structural Depth Studies

## Lateral Analysis and Design

### Existing Braced Frame 5 & 6

Level	Column	Brace	Girder
1 - 3	W14x665	HSS 8x8x3/8	W24x84
4-7	W14x605	HSS 10x8x3/8	W24x94
7-10	W14x455	HSS 10x8x3/8	W24x94
11-14	W14x342	HSS 16x8x1/2	W24x94

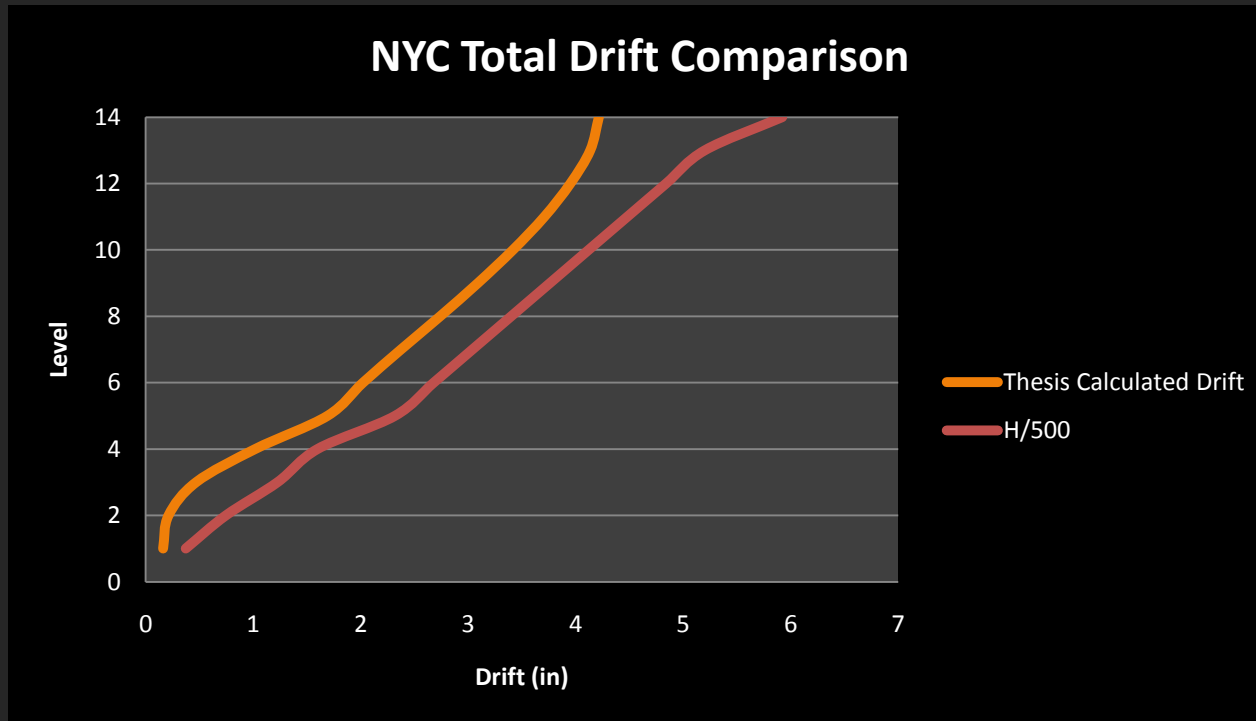
### Re-designed Braced Frame 5 & 6

Level	Column	Brace	Girder
1 - 3	W14x500	HSS 8x8x3/8	W24x84
4-7	W14x730	HSS 8x8x3/8	W24x94
7-10	W14x370	HSS 8x8x3/8	W24x94
11-14	W14x159	HSS 12x8x3/8	W24x94

# Structural Depth Studies

## Lateral Drift – New York City Building Code

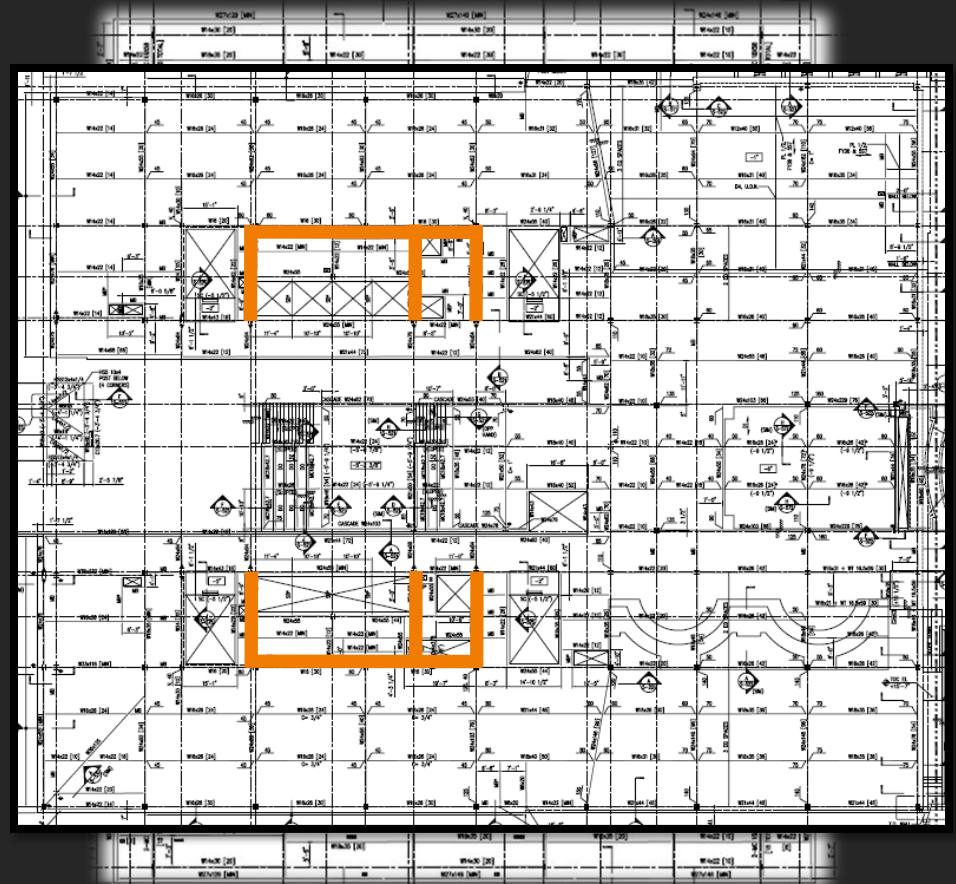
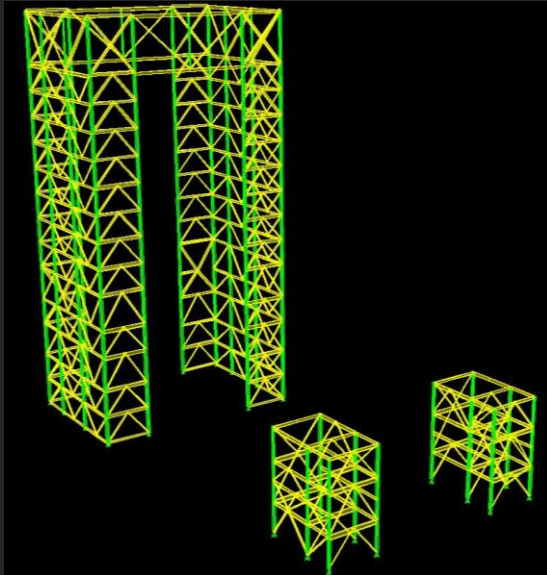
- Necessary to compare re-design to the original design criteria



# Existing Structural Systems

## Lateral Force Resisting System

- Concentrically Braced Frame Core
  - Braces range from HSS 6x6x3/8" to HSS 16x8x1/2"





# Construction Management Breadth Studies

## Weight Comparison

System	Thesis (kips)	Existing (kips)
Trusses	1380	1521
Perimeter Columns/Plate hangers	112	107
Braced Frame Core	1324	1304
Built-Up Girders	235	294
<b>Total</b>	<b>3051</b>	<b>3226</b>

**New transfer system weighs 87 tons less than  
the existing design**

